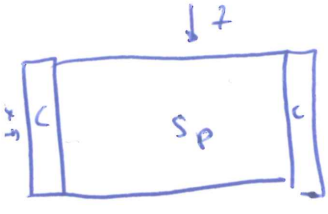


Calcolo modulo elastico di osso sano



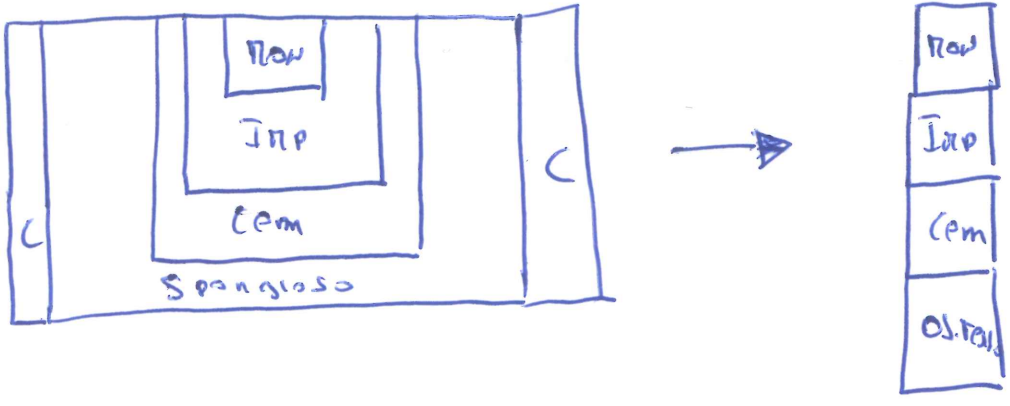
$$E_z^0 = f_c E_z^c + f_{sp} E_s = 0,83 \text{ GPa}$$

$$E_{xy}^0 = \frac{E_{xy}^c E_s}{f_c E_s + f_{sp} E_{xy}^c} = 0,51 \text{ GPa}$$

$$f_c = 27\%$$

$$f_{sp} = 98\%$$

Struttura con protesi:



poiché $f_{IIP} + f_{IIP} + f_{cem} + f_{os.residuo} = 1$ e f_{cem} molto piccola
lo trascuro

$$f_{IIP} + f_{IIP} + f_{os.res} = 1$$

$$E_{os.residuo}^z = E_0^z (1-p)^5 = E_0^z (1 - f_{IIP} - f_{IIP})^5$$

$$E_{os.residuo}^{xy} = E_0^{xy} (1-p)^5 = E_0^{xy} (1 - f_{IIP} - f_{IIP})^5$$

$$E_{TOT}^z \Rightarrow \left\{ \begin{array}{l} \frac{1}{E_{TOT}^z} = \frac{f_{pov}}{E_{pov}} + \frac{f_{imp}}{E_{imp}} + \frac{f_{os.res}}{E_{os.res}^z} \\ E_{TOT}^{xy} = f_{pov} E_{pov} + f_{imp} E_{imp} + f_{os.res} E_{os.res}^{xy} \\ f_{pov} + f_{imp} + f_{os.res} = 1 \end{array} \right.$$

$$\left\{ \begin{array}{l} \frac{1}{E_0^z} = \frac{f_{pov}}{E_{pov}} + \frac{f_{imp}}{E_{imp}} + \frac{(1 - f_{pov} - f_{imp})}{E_0^z (1 - f_{pov} - f_{imp})^5} \\ E_0^{xy} = f_{pov} E_{pov} + f_{imp} E_{imp} + (1 - f_{pov} - f_{imp}) E_0^{xy} (1 - f_{pov} - f_{imp})^5 \\ f_{os.res} = 1 - f_{pov} - f_{imp} \end{array} \right.$$

$$\left\{ \begin{array}{l} \frac{1}{E_0^z} \left[1 - \frac{1}{(1 - f_{pov} - f_{imp})^5} \right] = \frac{f_{pov}}{E_{pov}} + \frac{f_{imp}}{E_{imp}} \\ E_0^{xy} = f_{pov} E_{pov} + f_{imp} E_{imp} + E_0^{xy} (1 - f_{pov} - f_{imp})^5 \\ f_{os.res} = 1 - f_{pov} - f_{imp} \\ E_{pov} = 2 E_{imp} \end{array} \right.$$

$$\left. \frac{1}{E_0^2} \left[1 - \frac{1}{(1 - f_{\text{KOW}} - f_{\text{IHP}})^4} \right] = \frac{f_{\text{KOW}}}{2E_{\text{IHP}}} + \frac{f_{\text{IHP}}}{E_{\text{IHP}}} = \frac{f_{\text{KOW}} + 2f_{\text{IHP}}}{2E_{\text{IHP}}} \right\}$$

$$E_0^{xy} = 2f_{\text{KOW}} E_{\text{IHP}} + f_{\text{IHP}} E_{\text{IHP}} + E_0^{xy} (1 - f_{\text{KOW}} - f_{\text{IHP}})^6$$

$$E_0^{xy} = E_{\text{IHP}} (2f_{\text{KOW}} + f_{\text{IHP}}) + E_0^{xy} (1 - f_{\text{KOW}} - f_{\text{IHP}})^6$$

$$f_{\text{OS}} = 1 - f_{\text{KOW}} - f_{\text{IHP}} \quad E_{\text{KOW}} = 2E_{\text{IHP}}$$

$$\left. 1 - \frac{1}{(1 - f_{\text{KOW}} - f_{\text{IHP}})^4} = \frac{E_{\text{OZ}}}{2E_{\text{IHP}}} (f_{\text{KOW}} + 2f_{\text{IHP}}) \right\}$$

$$E_0^{xy} \left[1 - (1 - f_{\text{KOW}} - f_{\text{IHP}})^6 \right] = E_{\text{IHP}} (2f_{\text{KOW}} + f_{\text{IHP}})$$

$$f_{\text{OS}} = 1 - f_{\text{KOW}} - f_{\text{IHP}} \quad E_{\text{KOW}} = 2E_{\text{IHP}}$$

$$1 - 0,004 (f_{\text{KOW}} + 2f_{\text{IHP}}) = \frac{1}{(1 - f_{\text{KOW}} - f_{\text{IHP}})^4}$$

$$\Rightarrow (1 - f_{\text{KOW}} - f_{\text{IHP}})^4 = \frac{1}{1 - 0,004 (f_{\text{KOW}} + 2f_{\text{IHP}})}$$

$$E_0^{xy} \left[1 - (1 - f_{\text{KOW}} - f_{\text{IHP}})^4 (1 - f_{\text{KOW}} - f_{\text{IHP}})^2 \right] = E_{\text{IHP}} (2f_{\text{KOW}} + f_{\text{IHP}})$$

$$1 - \frac{1}{1 - 0,004 (r_{\text{πω}} + 2r_{\text{ΓΠρ}})} \cdot (1 - r_{\text{πω}} - r_{\text{ΓΠρ}})^2 = \frac{r_{\text{ΓΠρ}}}{r_{\text{ωγ}}} (2r_{\text{πω}} + r_{\text{ΓΠρ}})$$

$$1 - \frac{(1 - r_{\text{πω}} + r_{\text{ΓΠρ}} - 2r_{\text{πω}} - 2r_{\text{ΓΠρ}} + 2r_{\text{πω}}r_{\text{ΓΠρ}})}{1 - 0,004 (r_{\text{πω}} + 2r_{\text{ΓΠρ}})} = 196 (2r_{\text{πω}} + r_{\text{ΓΠρ}})$$

$$1 - 0,004 r_{\text{πω}} - 0,008 r_{\text{ΓΠρ}} - 1 + r_{\text{πω}} - r_{\text{ΓΠρ}} + 2r_{\text{πω}} + 2r_{\text{ΓΠρ}} + 2r_{\text{πω}}r_{\text{ΓΠρ}} = 392 r_{\text{πω}} + 196 r_{\text{ΓΠρ}}$$

$$- r_{\text{πω}} - r_{\text{ΓΠρ}} + 2r_{\text{πω}}r_{\text{ΓΠρ}} - 390 r_{\text{πω}} - 194 r_{\text{ΓΠρ}} = 0$$

$$r_{\text{πω}} + r_{\text{ΓΠρ}} + 2r_{\text{πω}}r_{\text{ΓΠρ}} + 390 r_{\text{πω}} + 194 r_{\text{ΓΠρ}} = 0$$

~~$$r_{\text{πω}} + r_{\text{ΓΠρ}} + 2r_{\text{πω}}r_{\text{ΓΠρ}} + 390 r_{\text{πω}} + 194 r_{\text{ΓΠρ}} = 0$$~~

$$r_{\text{πω}} + (390 - 2r_{\text{ΓΠρ}}) r_{\text{πω}} + (194 r_{\text{ΓΠρ}} + r_{\text{ΓΠρ}}^2) = 0$$

$$r_{\text{πω}} = - (390 - 2r_{\text{ΓΠρ}}) \pm \frac{\sqrt{(390 - 2r_{\text{ΓΠρ}})^2 - 4 (194 r_{\text{ΓΠρ}} + r_{\text{ΓΠρ}}^2)}}{2}$$

$$r_{\text{πω}} = - (390 - 2r_{\text{ΓΠρ}}) \pm \frac{\sqrt{52100 + 4r_{\text{ΓΠρ}}^2 - 156r_{\text{ΓΠρ}} - 776 r_{\text{ΓΠρ}} - 4r_{\text{ΓΠρ}}^2}}{2}$$

$$f_{\text{row}} = \frac{-(390 - 2f_{\text{IHP}}) + \sqrt{152100 + 2336 f_{\text{IHP}}}}{2}$$

~~...~~

$$f_{\text{row}} = \frac{-(390 - 2f_{\text{IHP}}) + 390}{2}$$

$$f_{\text{row}}^1 = \frac{-390 + 2f_{\text{IHP}} + 390}{2} = f_{\text{IHP}}$$

$$f_{\text{row}}^1 = \frac{-390 + 2f_{\text{IHP}} - 390}{2} = f_{\text{IHP}} - 390 \quad \text{non ammissible}$$

$$f_{\text{row}} = f_{\text{IHP}}$$

$$\left\{ \begin{array}{l} E_0^{xy} = \underline{E_{\text{IHP}}} \cdot 3 f_{\text{IHP}} + E_0^{xy} (1 - 2f_{\text{IHP}})^6 \\ 1 - \frac{1}{(1 - 2f_{\text{IHP}})^4} = \frac{E_0 +}{2E_{\text{IHP}}} (3 f_{\text{IHP}}) \Rightarrow 0,017 f_{\text{IHP}} - 1 = \frac{1}{(1 - 2f_{\text{IHP}})^4} \end{array} \right.$$

$$(1 - 2f_{\text{IHP}})^4 = \frac{1}{(0,017 f_{\text{IHP}} - 1)}$$

$$(1 + 8f_{\text{IHP}} + 24f_{\text{IHP}}^2 + 32f_{\text{IHP}}^3 + 16f_{\text{IHP}}^4) = \frac{1}{(0,017 f_{\text{IHP}} - 1)}$$

6

$$\begin{aligned}
 & [0,012 f_{\text{TPP}} - 1 - 0,096 f_{\text{TPP}}^2 + 8 f_{\text{TPP}} + 0,288 f_{\text{TPP}}^3 - 24 f_{\text{TPP}}^4 + \\
 & -0,384 f_{\text{TPP}}^4 + 32 f_{\text{TPP}}^3 + 0,192 f_{\text{TPP}}^5 - 16 f_{\text{TPP}}^4 = \phi \\
 & \quad \quad \quad + \quad \quad \quad + \quad \quad \quad + \quad \quad \quad +
 \end{aligned}$$

$$\begin{aligned}
 & 0,192 f_{\text{TPP}}^5 - 16,384 f_{\text{TPP}}^4 + 32,283 f_{\text{TPP}}^3 - 24,096 f_{\text{TPP}}^2 + 24,012 f_{\text{TPP}} - \\
 & - 2 = \phi
 \end{aligned}$$

Il sistema prevede 5 soluzioni reali e 4 complesse e immaginarie,
 Il fatto che 4 siano complesse e immaginarie vuol dire che l'approssimazione fatta
 sul campo è un po' forte, comunque considero solo lo parte reale.

$$f_{\text{TPP}} = 0,14$$

$$f_{\text{TPP}} = 0,14$$

$$f_{\text{os.res}} = 1 - 0,28 = 0,72$$

Dubb

I problemi sono legati che se le due parti presentano E diversi equando
 avviene sia coeff. di attrito diverso o quindi fenomeni di Debus
 sia caudici o zottino dresi.

Punto a - Vedere appunti in rete

Punto b.

Il rumore termico $k_B T$ è simile al rumore bianco con

Spettro di potenza costante nel range del parlato.

Sia che il rumore sia additivo che moltiplicativo, essendo

lo spettro del sistema del parlato, portando il segnale x

oltre lo scope del dolore e quindi il parlato non è

nullo e non dolore.